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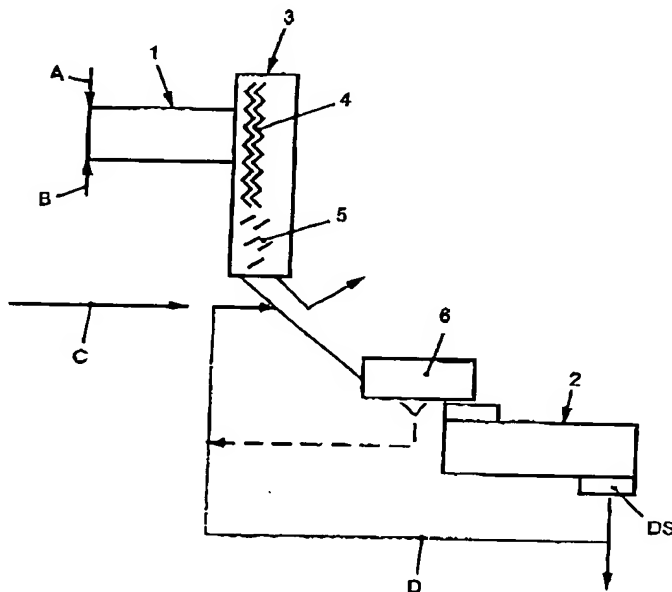
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(54) Title: PROCESS FOR THE PRODUCTION OF SAP



(57) Abstract: In a continuous process for the production of dried Supraabsorbent polymers (SAPs) the polymerization reaction is carried out either in an initially homogenous aqueous monomer solution (bulk aqueous solution polymerization) or in a heterogeneous water-in-oil reactant mixture (reverse phase suspension or emulsion polymerization) within a continuous closed polymerization reactor (1), then the resulting polymer gel is dried within a continuous moved bed in a closed dryer (2), avoiding the needs of standard intermediate maturity tank(s).

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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

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Process for the production of SAP

This Invention relates to an improved continuous process for the production of Superabsorbent Polymers, referred hereafter, as SAPs. More particularly, this invention relates to such process in which a continuous closed polymerisation reactor is combined with a continuous moved bed and closed dryer, avoiding the needs of standard intermediate maturity tank(s) and allowing condensing then recycling of residual reactants, additives and/or solvents.

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1. INTRODUCTION

SAPs are polymers capable to absorb tens to several hundred times their own weight of liquid. Examples of liquids that could be absorbed are water, urine, blood, aqueous solutions of salts, fertilizers, pesticides, inks, etc.

SAPs are utilized in various applications that include personal care articles (diapers, napkins, etc.), agriculture, horticulture, transportation for perishable goods, fire fighting, communication cables, drug delivery, etc..

Polymerization

The polymerization reaction to produce SAPs can be carried out either in aqueous and initially homogenous phase (bulk solutions polymerization) or in water-in-oil and therefore heterogeneous phase (reverse emulsion or reverse suspension polymerizations). In this latter case, usually, the presence of at least one surfactant and/or other emulsion stabilizer(s) is necessary.

1. Bulk aqueous solution polymerization: An aqueous and homogenous reactant(s) mixture is initially prepared. Generally, water is the only solvent present in the mixture with a concentration between 15% and 90%. But the reaction could also be carried out in the presence of at least one additional solvent. As the polymerization is taking place, the reaction mixture becomes more and more viscous and a gelly SAP is progressively formed.

2. Reverse phase suspension or emulsion polymerizations (referred hereafter as Suspension Polymerization, for commodity): In these cases, two phases are present in the reaction mixture: An organic continuous phase and an aqueous discontinuous phase (droplets), in which the (co)monomers and other reactants and additives are dissolved. Generally, at least one suspending agent such as surfactants are usually used to stabilize the heterogeneous mixture. Compared to solution polymerization, the suspension polymerization leads to less viscous reaction media and better heat transfer.

For the abovementioned two ways, the polymerization is generally carried out under partial vacuum and/or mostly under inert condition, i.e. in the presence of inert gas.

Various types of reactants and materials can be utilized to obtain SAPs:

- SAPs are generally produced by (co)polymerization of at least one water-soluble monoethylenically unsaturated monomer, and/or at least one waterinsoluble monoethylenically unsaturated monomer that can be totally or partly transformed to a water-soluble one by chemical modification(s), in the presence of at least one crosslinker, initiator, and, usually, other additives. These types of SAP are crosslinked networks of flexible polymer chains. Crosslinked poly(meth)acrylic acids and partially or totally neutralized poly(meth)acrylic acids, poly(meth)acrylamides and

partial or total hydrolyzates of poly(meth)acrylamide, polyvinyl alcohol or poly(allylamines) are few examples of efficient SAPs.

5

- Another way to produce SAPs is to allow the polymerization of at least one water-soluble monoethylenically unsaturated monomer(s) in the presence of at least one water-soluble, natural or synthetic, polymer (WSP) such as epoxide polymers, polysaccharides (ex. cellulose, starch, gums, etc.), polyvinyl alcohol and/or their derivatives. In this case the result is either a grafted, block or esterified SAP. In the reaction mixture, one may also add at least one crosslinker, other additives or a combination thereof. Polysaccharides-graft copolymers with acrylonitrile, (meth)acrylic acids and their salts (meth)acrylamides and their hydrolyzates are some examples of that types of SAP.

20

- Also another way to prepare SAP is to carry at least one modification on functional groups of already available natural or synthetic polymers. One modification consists on crosslinking branching, and/or grafting reactions or a combination thereof on at least one WSP. Another modification could be partial or total neutralization or hydrolysis of already crosslinking absorbent polymers.

30

Post-treatment of SAPs

In various cases, the SAP, which is already transformed into gel crumbles or dried granulated, could also be post-treated (a post-treatment step). During this step, one or more reactants or additives such as water, SAP properties improved additives, surface crosslinker, initiators, or a combination thereof, are added to the SAP crumbles. The post-treatment could be effected in atmospheric, vacuum, or inert conditions and in the presence or absence of heating. The SAP may also be post-treated by heat, in atmospheric, vacuum or inert conditions without addition of any material.

The post-treatment step allows reaching one or more objectives for SAPs and/or process properties. One of the objectives to post-treat SAP is to increase the process efficiency such as recycling the dry SAP fines or allowing the reaction to proceed at higher conversion by holding the polymer for a longer time at higher temperature and/or adding additional initiators. Another objective of post-treatment is to improve one property or more of the SAP. Examples of such properties to be improved are gel strength (by increasing surface crosslinking), swelling capacity, absorption rate, stability to urine, salts and UV, rate of moisture absorption in humid environments, contents of residual monomers, contents of unwanted soluble polymers in SAP, degree of fines, etc.

Example of Reactants and Components for SAP Productions

Water-soluble monoethylenically unsaturated monomers

5

Any monomer, its salts, hydrolysats, derivatives or a combination thereof that is partly or totally miscible with water and that yields, after (co)polymerization, SAPs or polymers that can be transformed by hydrolysis or neutralization into SAPs.

10

Example of water-soluble monoethylenically unsaturated monomers used for preparing SAPs include α , β -ethylenically unsaturated carboxylic acid such as (meth)acrylic acid, maleic acid, maleic anhydride, fumaric acid, crotonic acid, citraconic acid, their esters (ex. (meth)acrylates of Methyl, ethyl, N-butyl, 2-hydroxyethyl, etc.), their N-substituted (alkyl)amides (ex. (meth)acrylamide, N-methylacrylamide, N-terbutylacrylamide, N,N-dimethylacrylamide, etc.), or their alkali metal and/or ammonium salts (ex. sodium (meth)acrylate, potassium(meth)acrylate, ammonium (meth)acrylate, etc.)

15

20

Other examples of water-soluble monoethylenically unsaturated monomers used for preparing SAPs include monomers containing nitrile group (ex. (meth)acrylonitrile, etc.), sulfo group (vinyl sulfonic acid, etc.), esters obtained by reaction of organic oxides (ethylene oxide, propylene oxide, etc.) or carboxylic acids with alcohols and there derivates.

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Other examples of water-soluble monoethylenically unsaturated monomers used for preparing SAPs include (meth)acroleine, vinyl acetate, vinyl propionate, N-vinylpyrrolidone, N-vinylformamide, N-vinylcaprolactame and
5 their derivatives.

A combination of two or more of the above-mentioned water-soluble monoethylenically unsaturated monomers and their derivatives can also be used.

10

CROSSLINKERS

Any type of organic crosslinking agent, inorganic crosslinking agent or a combination thereof that are
15 already used for preparing SAPs.

Organic crosslinkers: molecules having two or more polymerizable double bonds per molecular unit. This includes diethylene, triethylene, propylene and neopentyl
20 glycols; 1,4-butane diol; 1,5-pentane diol; 1,6-hexane diol; N,N'-methylene-bis-(meth)acrylamide; di(meth)acrylate of ethylene glycol; triallyl isocyanurate; tetra(meth)acrylates of pentaerythritol; trimethylol propane and pentaerythritol; and triacrylates of trimethacrylates
25 of trimethylol propane and pentaerythrol.

Nonvinyl crosslinkers such as glycerol, polyethyleneglycols, ethyleneglycol diglycidyl ether and a combination thereof could also be used. Their combination
30 with vinylic crosslinkers is also possible.

Inorganic crosslinkers: Examples of those agents are multivalent metallic cation solutions such as of Aluminium, Silicon, Titanium, Iron, etc..

- 5 One more of these Inorganic crosslinkers can be used in combination with one or more organic crosslinking agent.

Water-soluble polymers used for production of SAPs

- 10 Any natural or synthetic polymer or a combination thereof that is water-soluble or becomes partly or totally water-soluble after neutralization, hydrolysis, and/or other modifications(s) of their functional group(s) and that can be transformed to SAPs by crosslinking, grafting, blending,
15 compounding, or a combination thereof. Examples of such polymers are poly(meth)acrylic acids, poly(meth)acrylate, poly(meth)acrylamide, Polysaccharides (ex. cellulose, starch, gums, alginates, etc.), epoxide polymers, Poly(meth)acrylonitrile, polyvinyl alcohol, etc..

20

Initiators: Any type of initiator or a combination thereof, preferably thermal or redox initiators.

- 25 Additives: Any additive or a combination of additives that can improve SAPs properties, composition, and/or process efficiency.

- 30 Surfactants: Any surfactant or combination of surfactants that is already used in suspension or emulsion polymerization to produce SAPs.

II. SAPs Production (Reaction and Drying)

A method for the continuous production of SAPs as describe
in part I, which method comprises the continuous production
5 of hydrated (resp. suspended) free-flowing gel particles of
a given particle size, the eventual mixing of one or more
additives for their post-treatment and/or improving their
particles free-flowing properties, and the continuous
drying of these free-flowing hydrated (resp. suspended) gel
10 particles, wherein said dryer is characterized by a moved
product-bed. For the bulk solution polymerisation, this
method will replace the conventional moving belt reactors
and dryers, wherein the product remains motionless on a
moveable surface. For suspension polymerisation, the method
15 allows the use of higher monomer concentrations while
controlling efficiently the reaction and mixing parameters
and conserving a good product quality.

SAPs Produktion in List Reactors

20

The production and processing of SAPs according to the
description in paragraph I can be ideally and safely
carried out in one of the continuous twin-shaft kneader
reactors of the company List AG (ex. ORP-DP, CRP or CKR).
25 For example, during the course of polymerization when a SAP
is produced, the viscosity of the reaction mixture
increases as a gel is formed. The intermeshing of the
kneading elements, granulates this mass into small, uniform
free-flowing gel particles, which are discharged at a
30 conversion up to 90% or even more. Orientation angel of the
kneading elements assures the axial conveying of the pasty
polymer. The shape of kneading elements is an additional

parameter to adjust the compression or shear between the intermeshing zones.

The reaction can be carried out at any pressure.
5 Preferably, evaporative cooling can be used to remove the heat of reaction, especially when the autoacceleration of the reaction rate occurs (gel or Trommsdorff - Norrish effect). Depending on the degree of vacuum present into the reactor, approximately 0.5% to 40% or more of the water
10 and/or other solvent(s) is evaporated to remove the high reaction heat of the monomers (ex.: $\approx 70 \text{ KJ/mol}$ for the acrylates monomers). The condensed phase may contain traces or low concentrations of monomer(s) and additives. It may contain also surfactant(s) and/or other additives in the
15 case of suspension polymerization. The evaporated water or liquid mixture can be condensed, eventually separated then totally (reflux) or partly recycled in the reaction mixture (evaporative cooling). Alternatively, it can also totally be removed to dry partially the produced SAP crumbles.

20

Continuous Kneader Reactor

The List Kneader Reactor is particularly very suitable to produce SAPs since it is designed to improve the
25 radial/axial self - cleaning and axial conveying of viscous polymers, in addition to a good mixing during the reaction. Therefore, the system allows avoiding the complete filling/plugging of the reactor and the dead zones whilst working continuously. Torque is very important to the
30 compression zones, especially with regard to solid or gel particles. Since the SAP gels are very sensitive to the shear stress during their processing, this twin-shaft kneaders were optimized in order to avoid compression zones

between the barrel and the kneading elements, and the intermeshing zones of the kneading elements. At these conditions, no significant presence of squeezed or destroyed gels was observed, but a good and uniform quality of SAPs.

The above and other objects and advantages of novel features of the present invention will become apparent from the following detailed description of a preferred embodiment of the invention illustrated in the accompanying drawing which shows a schema of the invention.

As illustrative example, the case of a bulk solution polymerisation to produce SAPs is considered.

Polymerization Reaction:

Reactants and catalysts will be fed in a twin-shaft kneading reactor 1 by arrow A together with air, vapor or inert gas by arrow B.

The polymerization in solution or reverse phase suspension (or emulsion), as described in paragraph I, is conducted in the twin-shaft kneading reactor 1 (e.g. LIST-Reactor ORP-DP, CRP or CKR) in which the axial conveying is optimal and free flowing hydrated gel particles can be formed.

If, necessary, the gel particle size can be adjusted at the end of the twin shaft kneading reactor 1 and after discharge means 3 with a twin-screw 4 by means of adjustable knives 5. The cutting of the gel should be done at this wet stage (in vapor environment) in order to keep

the cut particles free flowing. The particle size at this stage of the continuous process is very important because of the drying efficiency, which is improved while processing small particles (diffusion controlled). For
5 example, SAPs particles of a diameter of 1 cm can be dried within 60 minutes or less at 180°C and 30 mbar.

Air, vapor or inert gas may be removed from the discharge means 3 after the knives.

10

Another possibility is the side discharge of free-flowing gel particles. In that case, a weir is then installed to regulate the fill level in the reactor. This option eliminates the needs of the discharge twin-screw.

15

Drying:

The SAP particles coming out of the twin-shaft kneading reactor 1 are already free-flowing particles because of the
20 humidity and eventually the presence of other component(s) or a combination thereof acting as a lubricant(s) on the surface of particles.

Trying to dry these hydrated gel particles directly in a
25 continuous moved-bed dryer 2 (e.g. rotary dryer, drum dryer, Discotherm dryer) results in a compactating of the hydrated gel particles because of the removing of the lubricant.

30 However, the mixing shown through arrow C of one or more appropriate additives or a combination thereof with the flow of hydrated gel particles coming out of the twin-shaft

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kneading reactor within a rotary mixer-tube 6 avoids the stickiness of the hydrated gel particles between each other while being separated from the superficial liquid film. These additives act as a free-flowing agent in the continuous dryer 2 wherein the product-bed is moved. The additive(s) could be in a powder or a liquid form, preferably as a powder. Examples of suitable additives or a combination thereof are kaolin, flour, talc, titanium dioxide, aluminium oxide, silica or the dried SAP fines D, which can be recycled at the end of the process and may be milled before being mixed as a free-flowing agent. However, any material or a combination of materials that are used in SAP post-treatments, as described in paragraph I, may also be employed as a free flowing agent while improving the polymer property, i.e. improved gel strength, absorption rate, reduced residual monomers, dust, etc. For SAPs used for agricultural and planting applications, liquid or powdery fertilizers, pesticides or a combination thereof, preferably in a powder form could be mixed with the hydrated gel particles and used as free-flowing agent during drying.

After the dryer 2 the dried SAPs are transferred to a not shown sieve.

25

The foregoing pre-drying mixing process can be carried out at atmospheric pressure or in presence of inert gas and/or vacuum. The presence of vacuum is preferred. Also for adjustment, the process may operate under vacuum by using List or any other commercial periphery systems.

30

The new method of drying is innovative compared to the usual continuous belt convective dryer. Based on the dryer

only, the financial impact is a considerable reduction of the drying investments when a moved-bed dryer is compared to a moving belt dryer wherein the product rests motionless on a movable surface. Moreover, by employing the moved-bed
5 dryer 2, particularly List dryers, the use of maturity tanks can be avoided.

The drying process can be carried out independently or in combination (cf. Fig. 1) with a twin-shaft kneading reactor
10 (e.g. List-Reactor ORP-PP, CRP or CKR), preferably in combination with the kneading reactor.

Each of the reactor 1 and the dryer 2 can be equipped with a condensing system. The discharge 3 includes a discharge
15 twin-screw 4 and adjustable knives 5 system, and is inserted between the twin-shaft kneading reactor 1 and the dryer 2. If necessary, a pressure lock chamber 7 may also be inserted between the reactor and the dryer. The pressure lock chamber 3 is particularly important when the reactor 1
20 and the dryer 2 are functioning at different pressures. Any pressure lock chamber present on the market can be used. The List system and the rotary valve system are particularly suitable as pressure lock chamber.

25 The process described above consisting on using of either the reactor 1 or the dryer 2 or the combination thereof has the advantages to be more efficient economically and environmentally and gives an improved product's quality since it has the benefits of being more compact (lower
30 space occupation), controlling better the reaction and drying parameters, avoiding the use of maturity tank(s), and giving the possibility to condense the evaporated solvents, and/or unreacted components then recycle them

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with larger recycling rate, which allows less residuals and gas wastes to be treated.

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WHAT IS CLAIMED IS:

1. A continuous process for the production of dried Superabsorbent polymers (SAPs) by carrying out the polymerization reaction, either in an initially homogenous aqueous monomer solution (bulk aqueous solution polymerization) or in a heterogeneous water-in-oil reactant mixture (reverse phase suspension or emulsion polymerization) within a continuous closed polymerization reactor (1), then drying of the resulting polymer gel within a continuous moved bed in a closed dryer (2), avoiding the needs of standard intermediate maturity tank(s).
2. A method according to claim 1, in which the moved bed closed dryer (2) consists of an agitated vessel having at least one agitating shaft, such shaft(s) being heated additionally to the vessel to increase the heat transfer and drying efficiency.
3. A method according to claim 2, in which the drying of the polymer is carried out under vacuum or in the presence of heated air, inert gas, steam or a combination thereof, preferably under vacuum.
4. A method according to claim 1 and 2, in which the maturity of the polymer, i.e reaction reaching very high conversion, is carried out into the first zone of the moved bed closed dryer (2).
5. A method according to claim 1, in which the mixing affect into either or both the closed continuous polymerization reactor (1) and the dryer (2) could be

used to incorporate, to the produced gel, one or more additional (co)monomers, additives (C) and solvents or a combination thereof.

- 5 6. A method according to claim 1, in which the mixing effect into either or both the closed continuous polymerization reactor (1) and the dryer (2) could be used to incorporate, to the produced gel, the recycled dry SAP fines that exit from the continuous discharge system (DS) and the sieve.
- 10
7. A method according to claim 1, in which either or both the continuous polymerization reactor (1) and the dryer (2) could be equipped with condensing and recycling systems of residual reactant(s), solvent(s) and additives or a combination thereof.
- 15
8. A method according to claim 7, in which the condensing and recycling systems of the continuous polymerization reactor (1) and the dryer (2) could be operated in an independent or combined way.
- 20
9. A method according to claim 7, in which the residual reactant(s), solvent(s) and additives or a combination thereof could be totally or partly recycled, together or separately at one or more locations of the continuous production process of claim 1.
- 25
10. A method according to claim 1, in which a pressure lock chamber (7) or a gel cutting system (5) or a combination thereof could be inserted between the continuous polymerization reactor (1) and the dryer (2).
- 30

11. A method according to claim 10, in which the type of
the pressure lock chamber is of any type of
commercially available pressure lock chambers,
5 preferably a rotary valve or a piston lock system.

12. A method according to claim 10, in which the pressure
lock chamber could be used to incorporate, to the
reaction mixture exiting the polymerization reactor,
10 one or more additional (co)monomers, additives and/or
solvents or a combination thereof.

13. A method according to claim 10, in which the type of
the gel cutting system is of any type of commercially
15 available cutting systems, preferably the Urshell
cutting system.

14. A method according to claim 10, in which the gel
cutting system could be used to incorporate one or more
20 additional (co)monomers, additives and solvents or a
combination thereof to the reaction mixture exiting the
polymerization reactor.

15. A method according to claim 14, in which the hydrated
25 get particles of a required size could be continuously
mixed with at least one additive improving free-flowing
and eventually other properties in a mixing screw or in
a rotary mixer-tube (6), which has a final portion with
holes allowing the additive(s) to be recycled before
30 entering the dryer (2).

16. A method according to claim 1 and 10, in which the
continuous polymerization reactor (1), the dryer (2)

and any device between them can function at equal pressure or different pressures.

15 17. A method according to claim 16, in which the continuous polymerization reactor (1), the dryer (2) and any device between them function under vacuum, preferably at different degrees of vacuum.

10 18. A method according to claim 17 and 10, in which the degree of vacuum into the dryer (2) is lower, preferably much lower than that in the continuous polymerization reactor (1) and the other devices between them.

15 19. A method according to claim 18 and 10, in which when the hot polymeric mixture enters the dryer (2), which is under much higher temperature and degree of vacuum than the polymerization reactor (1) and intermediate devices, the polymer is readily flashed leading to
20 intensive evaporation of solvent(s) and un-reacted components and hence to higher drying efficiency of the SAP, wherein the flash allows the SAP particles to be more porous and thus to have an increased liquid absorption rate.

25

20. A method according to claim 2 and 6, in which the hot and dry SAP particles exiting the dryer (2) can be partly cooled during their passage through the jacketed continuous discharge system (DS) such as cooling lock
30 vessel or other systems.

21. A method according to claim 1, 2 and 7, which method, compared to traditional processes for the SAPs

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production, has the advantage to yield less residual
reactant components and gas wastes to be treated.

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 European Patent Attorney

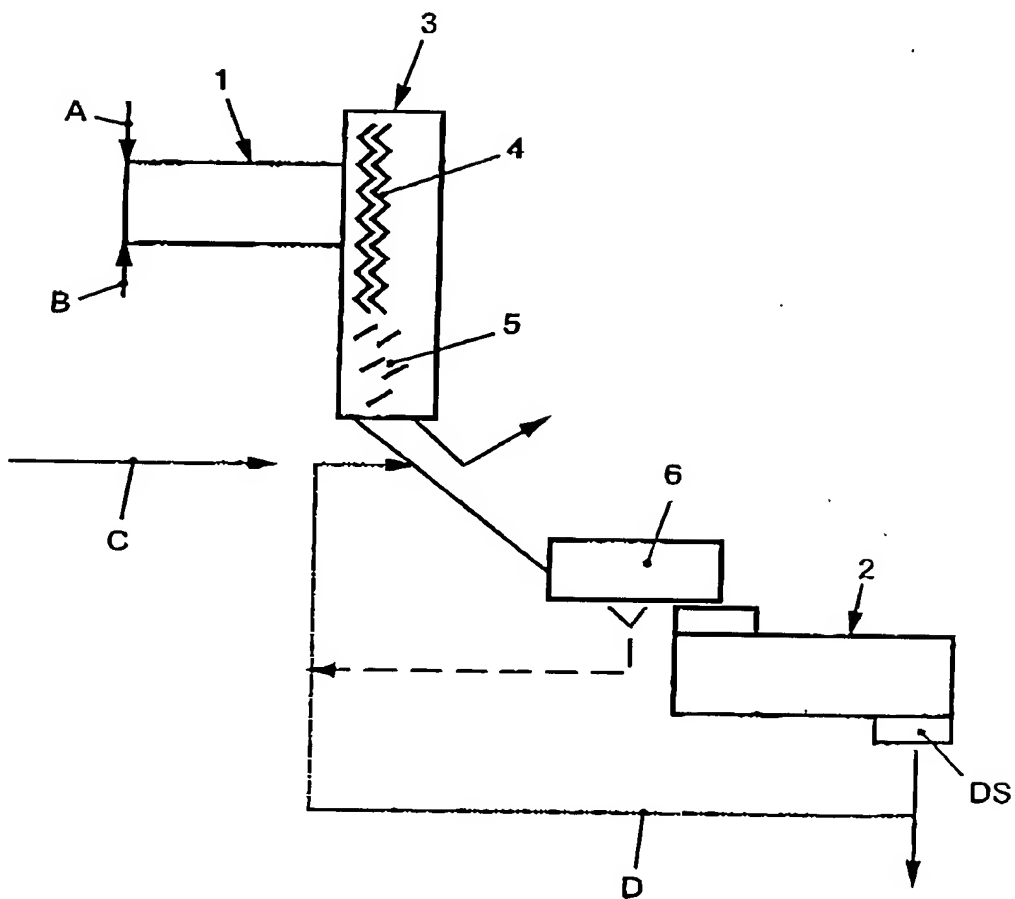
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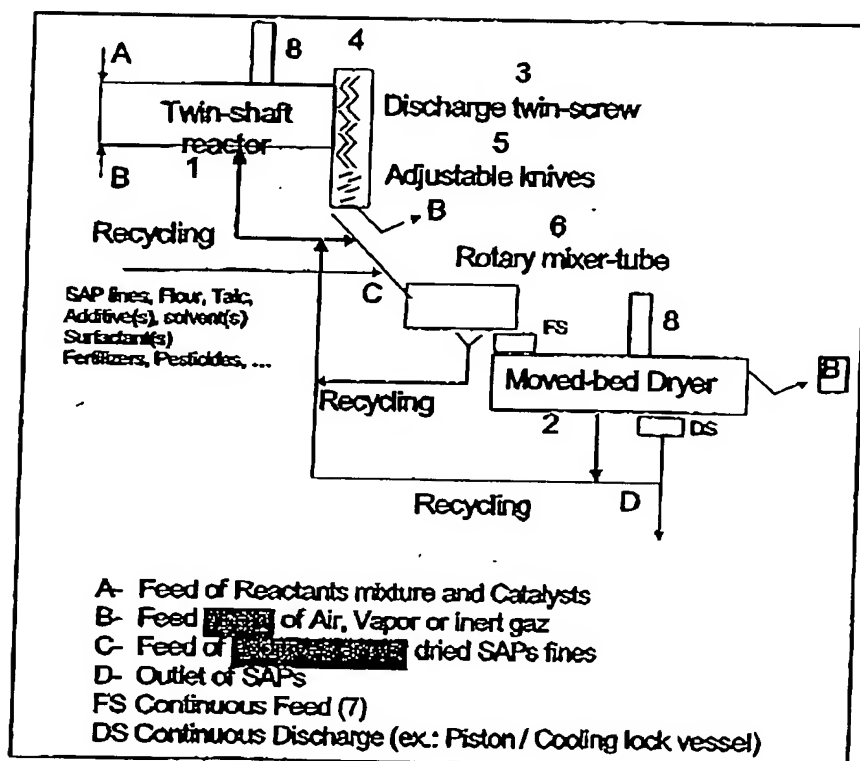
Aktenzeichen: P 2866/PCT

Datum: 22.08.2002 W/GE/HU

Positionszahlenliste

1	kneading reactor	34		67	
2	dryer	35		68	
3	discharge	36		69	
4	twin-screw	37		70	
5	knives	38		71	
6	mixer tube	39		72	
7	pressure lock chamber	40		73	
8	Condensing a/o reflux system	41		74	
9		42		75	
10		43		76	
11		44		77	
12		45		78	
13		46		79	
14		47			
15		48			
16		49		A	Feed of reactants a/o catalysts
17		50		B	Feed or removing air, vapor or inert gas
18		51		C	Feed of additives
19		52		D	SAP Fines recycling
20		53		FS	Feed system
21		54		DS	Discharge system
22		55			
23		56			





INTERNATIONAL SEARCH REPORT

International Application No.
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A. CLASSIFICATION OF SUBJECT MATTER

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According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 C08F C08L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5 668 252 A (T. YOKOI) 16 September 1997 (1997-09-16) -----	
A	US 3 634 944 A (M. ZONIS) 18 January 1972 (1972-01-18) -----	

☐ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

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